

# The Role of Computer Modelling in the Design, Optimisation and Operation of CP systems

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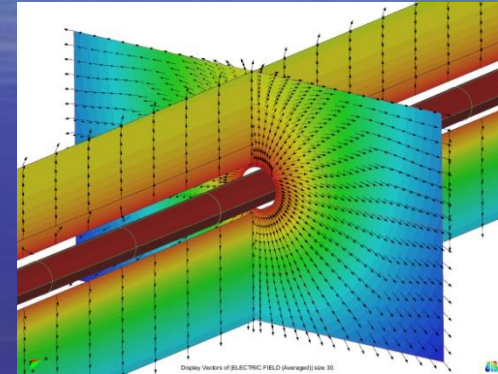
# Introduction

- Until computer-based mathematical simulation, achievement of required protection when designing a CP system relied on:
  - adherence to standards
  - skill and experience of the designer
- Computer simulation however now provides tools necessary to provide detailed *prediction* of protection levels
  - These tools can be used early in the design process, and can be used to optimise a design (whether SACP, ICCP, or a combined system)
  - Predictions can be used to help interpret data from surveys and monitoring



# Basis of mathematical modelling

- The simulation software determines:
  - Currents flowing through the electrolyte which may be seawater, ground, concrete
  - potential at any location in the electrolyte (eg survey positions, reference cell locations)
  - Potential and current density on the metal surfaces being protected
  - Magnitude of anode output
  - Anode remaining life
  - IR drop in long structures (pipelines, well casings etc)
  - Stray current or interference between different structures



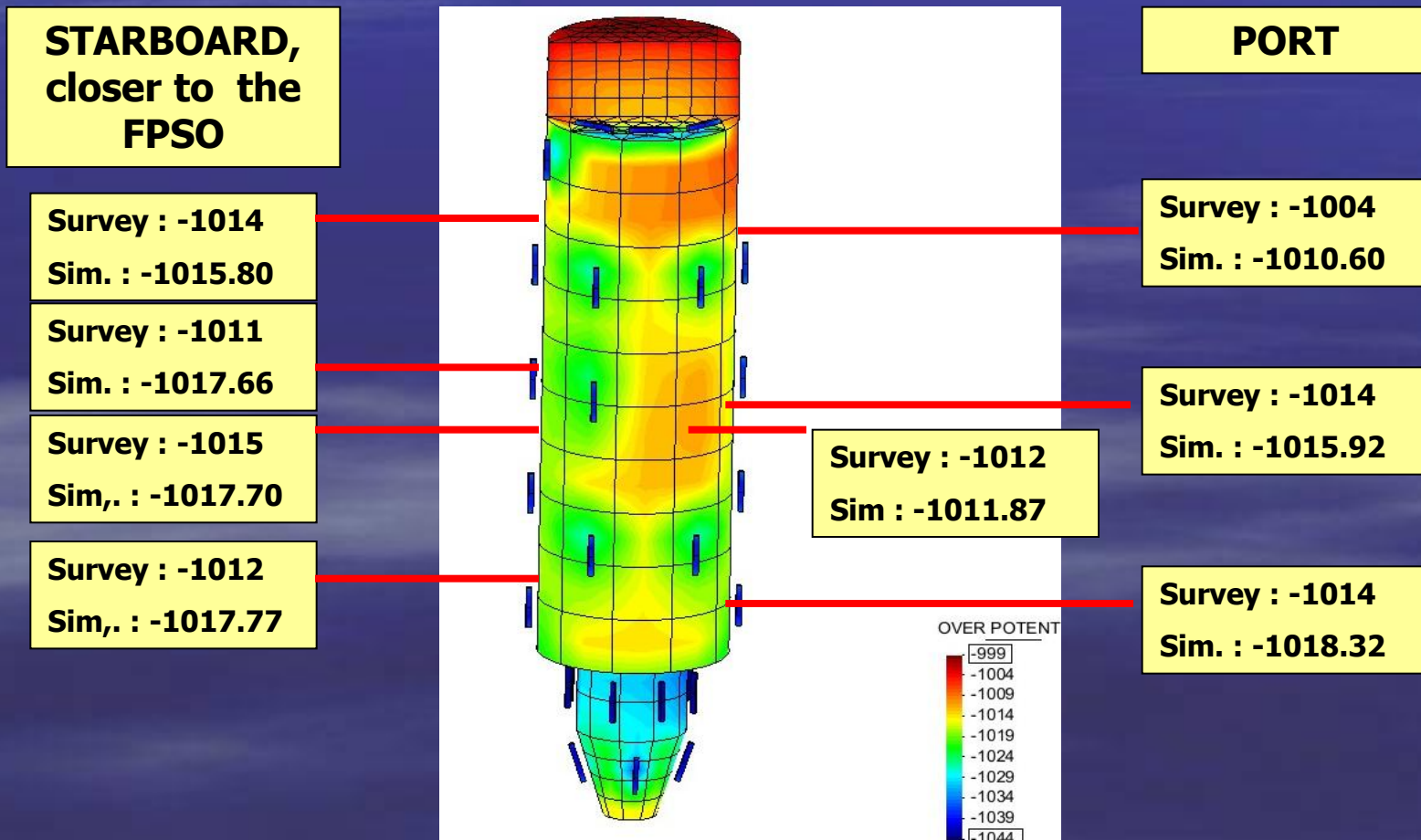
**Vectors showing current flow around an on-shore buried pipeline**

# Basis of mathematical modelling

- **The software:**
  - solves the Laplace equation in the electrolyte
  - Uses polarisation curves (long-term or potentiodynamic) on metal surfaces
  - Solves circuit equations in the return-path
- **By performing time stepping account can be taken of:**
  - Effects of changing coating breakdown factor
  - Anode mass loss and corresponding change of anode size
- **The software used in work reported in this paper is BEASY CP**

# Field surveys

- Simulation results can be used to gain confidence in survey data, and to extrapolate survey data to all parts of a structure

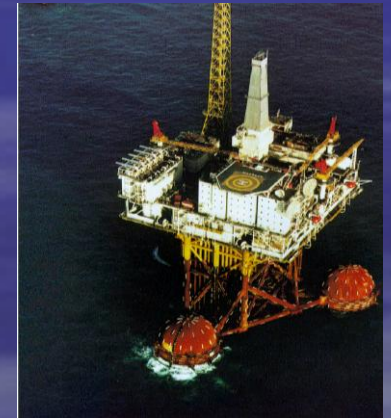
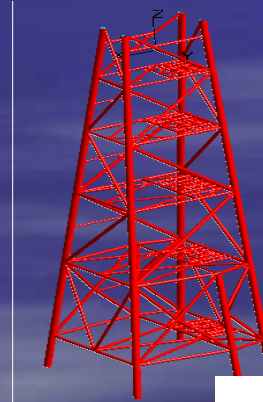
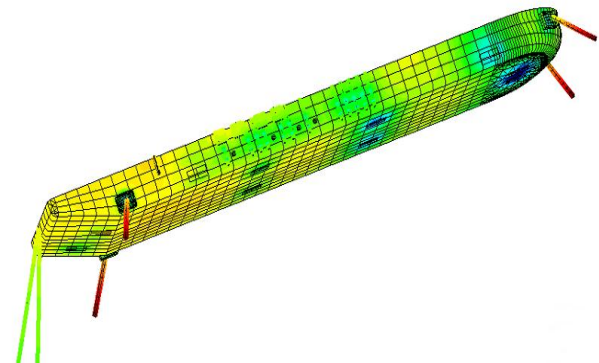


# Published data

- Extensive publications on simulation of CP systems in ships, offshore structures etc
  - where it has been used as an up-front design tool for optimisation of the CP system



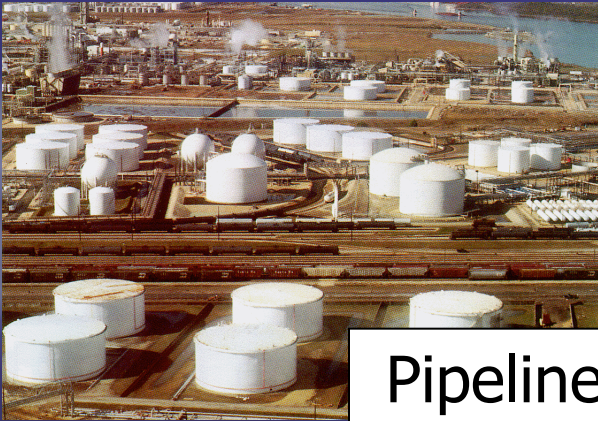
**Ships/  
FPSO's**



**Off-Shore  
Structures**

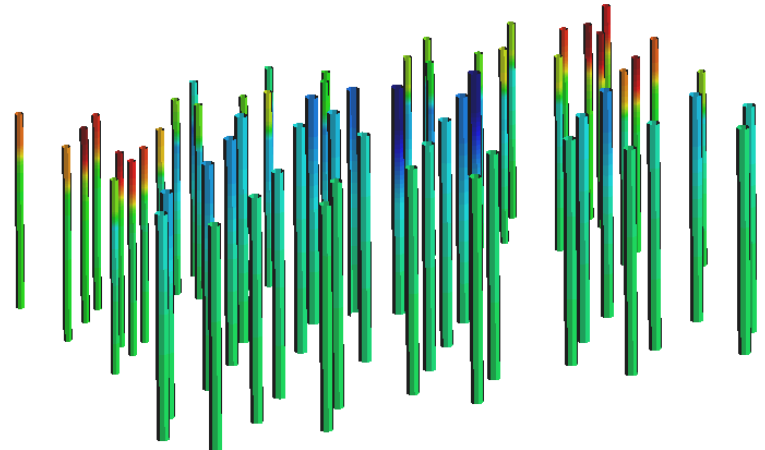
# Verified methodology

- As acceptance of accuracy of the methodology has been established, the experience has been extended to other structures, such as:
  - Storage tanks
  - Pipelines
  - Reinforced concrete



Pipelines, Storage tanks, Jetties, Pilings

Protection potentials on reinforced concrete pilings



# Asset operation and maintenance

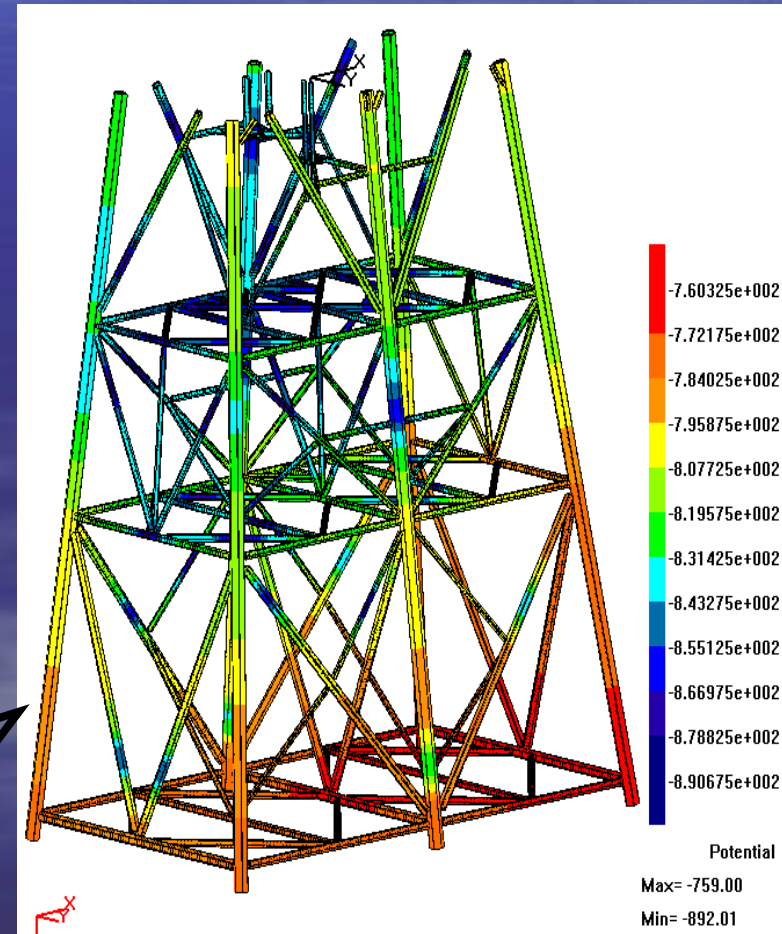
- **Simulation is developing as a means to support ongoing operation and maintenance of an asset**
  - Repeated simulation each year with calibration to annual survey to establish ongoing state of the asset
  - Prediction of best time to install retrofit CP systems (based on prediction of when existing anodes will be consumed)
  - Design of optimised retrofit CP system
  - Investigation of changes to the environment (new tie-ins, crossings etc)



# Asset operation and maintenance- Retrofit Design

- If localized or more general loss of calcareous deposits occurs, any retrofit SACP system will need to be able to produce the higher currents required to regenerate the calcareous deposits
- It is therefore financially beneficial to carefully time the installation of a retrofit system to avoid loss of calcareous deposits

**Potentials if previous anodes are consumed and calcareous deposits maintained by them are lost**



# Asset operation and maintenance- Retrofit Design

- It was decided that the retrofit system should be installed before the date when the previous system would expire
- This meant that calcareous deposits produced by the previous system would still be in place, and *could* be used to reduce the anode mass required in the retrofit

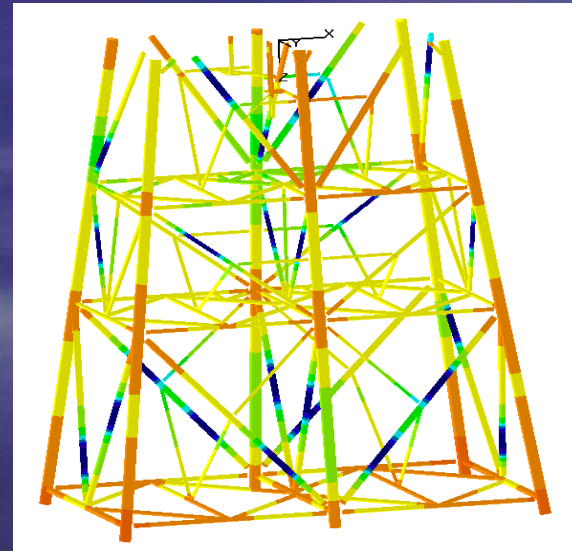
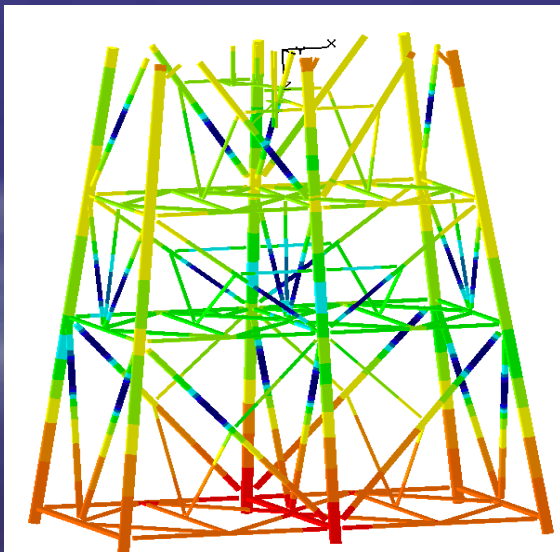
# Retrofit optimisation

- An initial anode layout was designed, then:
  - Performance was assessed
  - The results were used to guide anode position (and number) changes for the next, improved, design
  - Three or four such iterations produced a design with much better uniformity of potential and anode life



# Retrofit optimisation

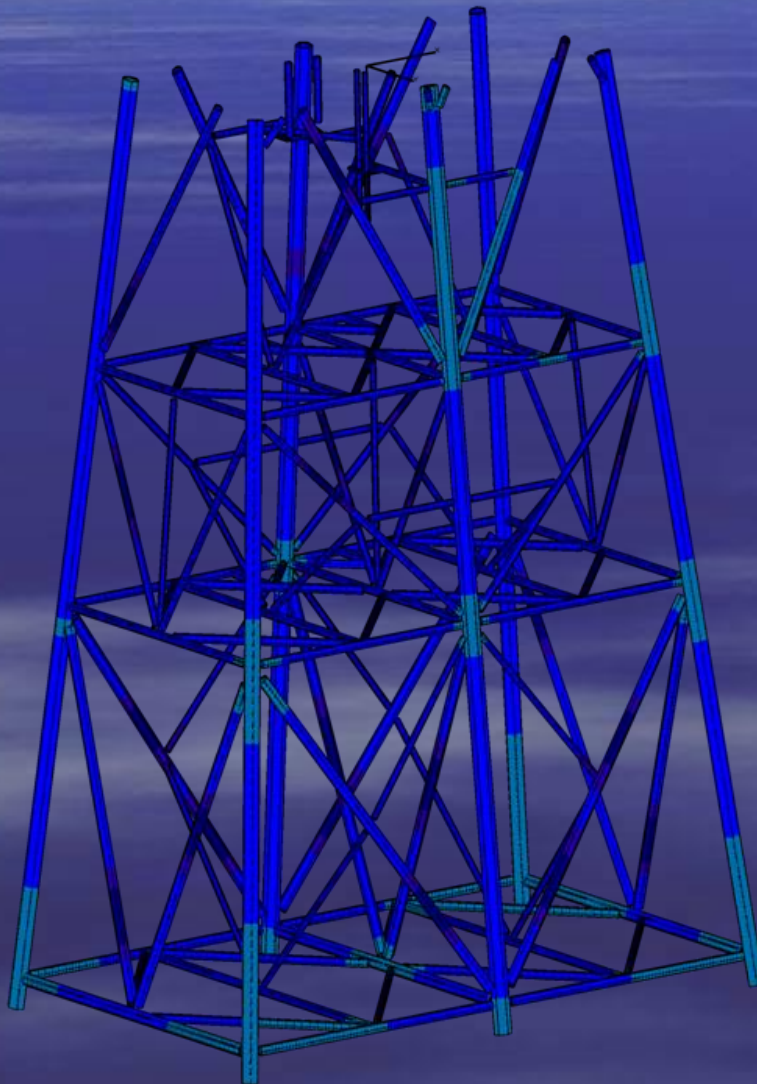
- **Structure potentials for two of the designs tested show greater variation over the structure for an early design (left) than for a later design (right)**



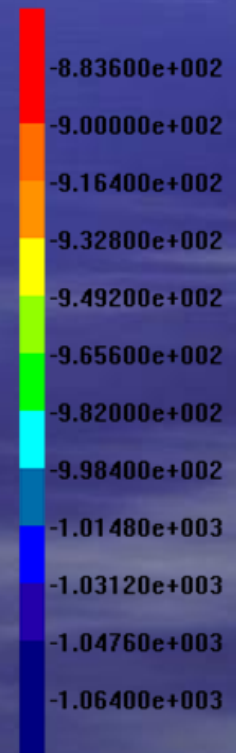
# Retrofit optimisation

- **Corresponding anode life projections made at end of life (after 15 years time stepping) showed:**
  - Anode life ranged from 9 to 14 years (design with 50 anodes)
  - Anode life ranged from 8 to 10 years (design with 46 anodes)
- **Data (remaining life/mass) is generated for each individual anode, and takes account of change of profile over time as it is consumed. Anodes reaching the defined utilisation factor are removed from the model.**

# New Retrofit: After Installation



**Blue  
indicates  
acceptable  
potentials**



Potential

Max= -1008.1

Min= -1060.9

# New Retrofit: After 15 Years



**Red indicates unacceptable potentials**



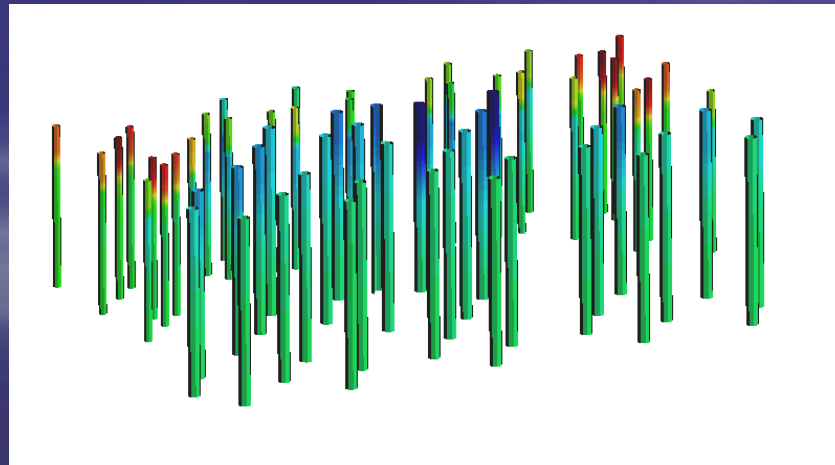
Potential

Max= -942.40

Min= -1004.4

# CP of steel in concrete

- CP systems for reinforced concrete, or steel piles coated in concrete, can be optimised using simulation
  - Design of an ICCP system applied to piles was optimised to control protection potentials



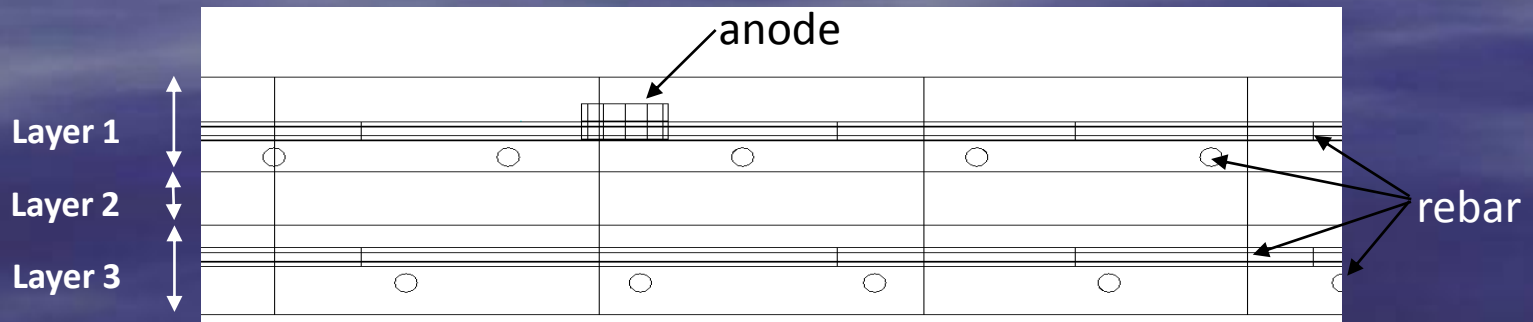


# CP of steel in concrete

- Retrofit CP systems to protect steel in concrete can be assessed and optimised
  - On a global scale (complete structures)
  - At a local scale (including individual reinforcement bars)

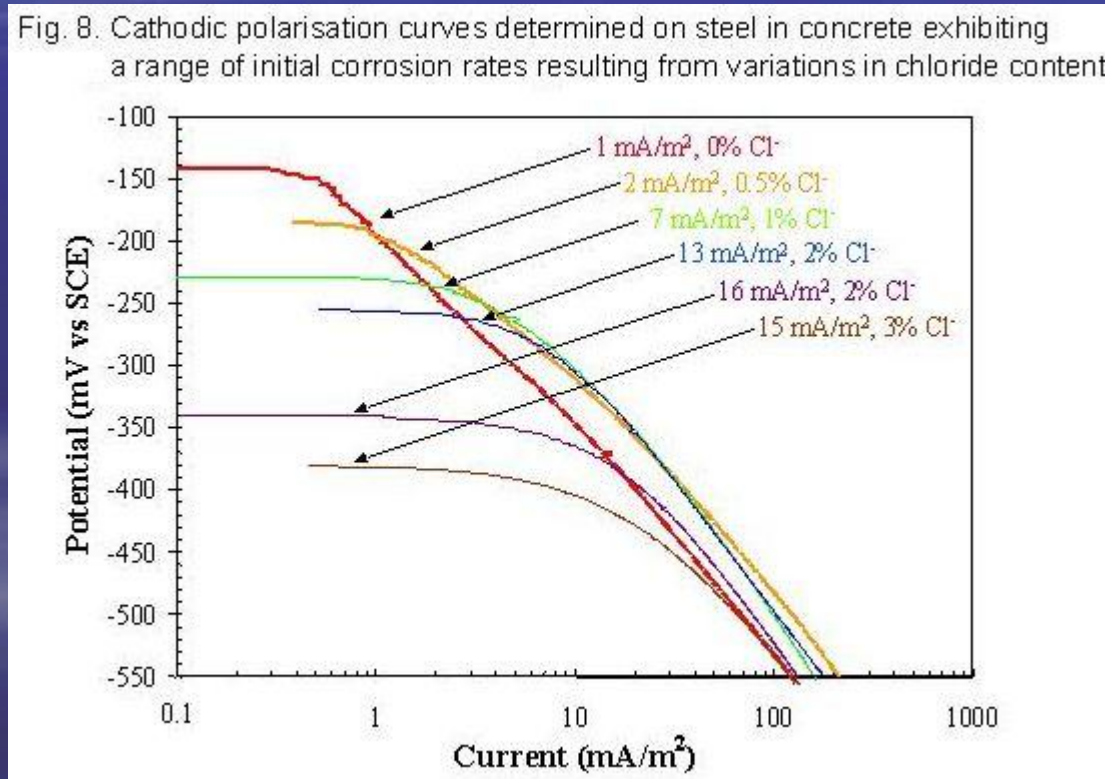
# CP of steel in concrete – local scale

- Investigation of potential distribution around single discrete anodes



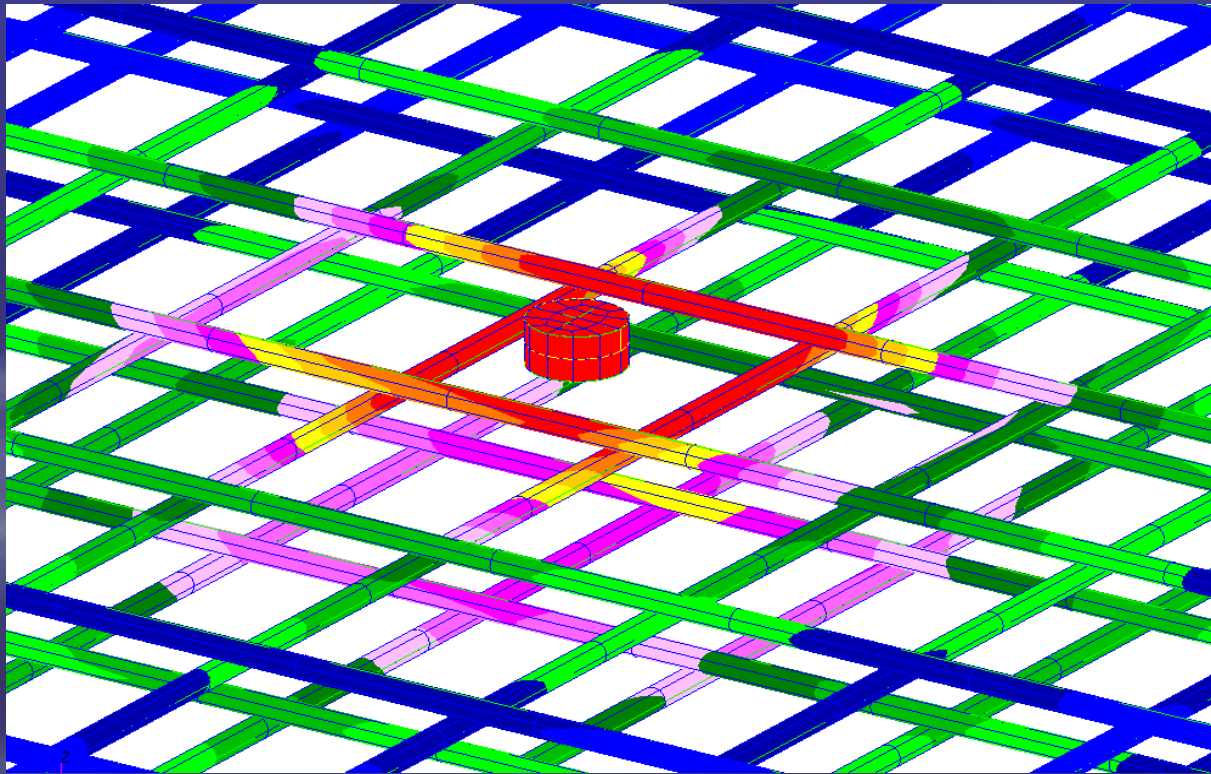
# CP of steel in concrete – local scale

- Various polarisation curves for reinforcement bars in different conditions



# CP of steel in concrete – local scale

- Potentials shown on individual reinforcement bars

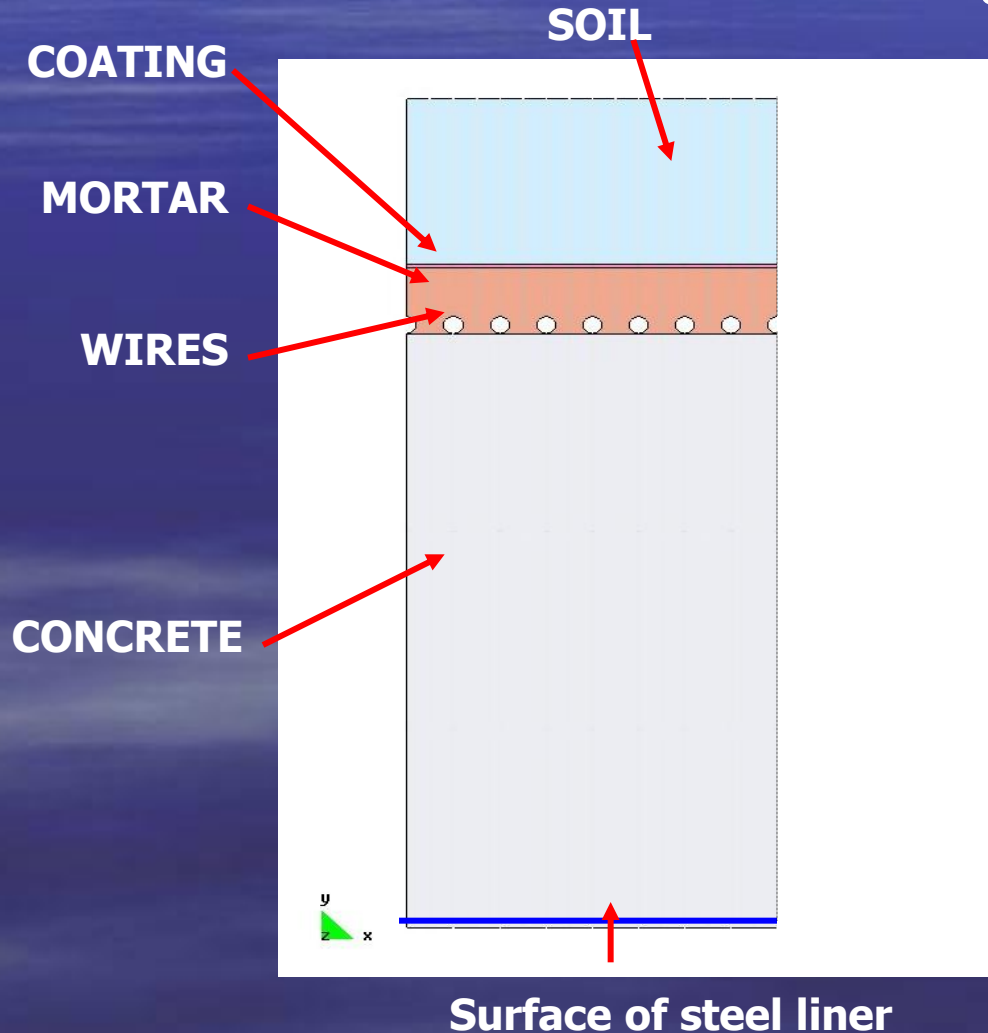


# CP of steel in concrete – global scale

- It is not feasible to include individual reinforcement bars in a large scale structure (100 metres or more)
- Instead:
  - A local model is used to determine properties which can be assigned to the surface of the concrete. This model includes:
    - Embedded steel
    - Rebars/wires
    - Concrete/mortar
    - Any coating on the surface of the mortar/concrete
  - The properties so-determined are then applied to surfaces in the large-scale model of the complete structure

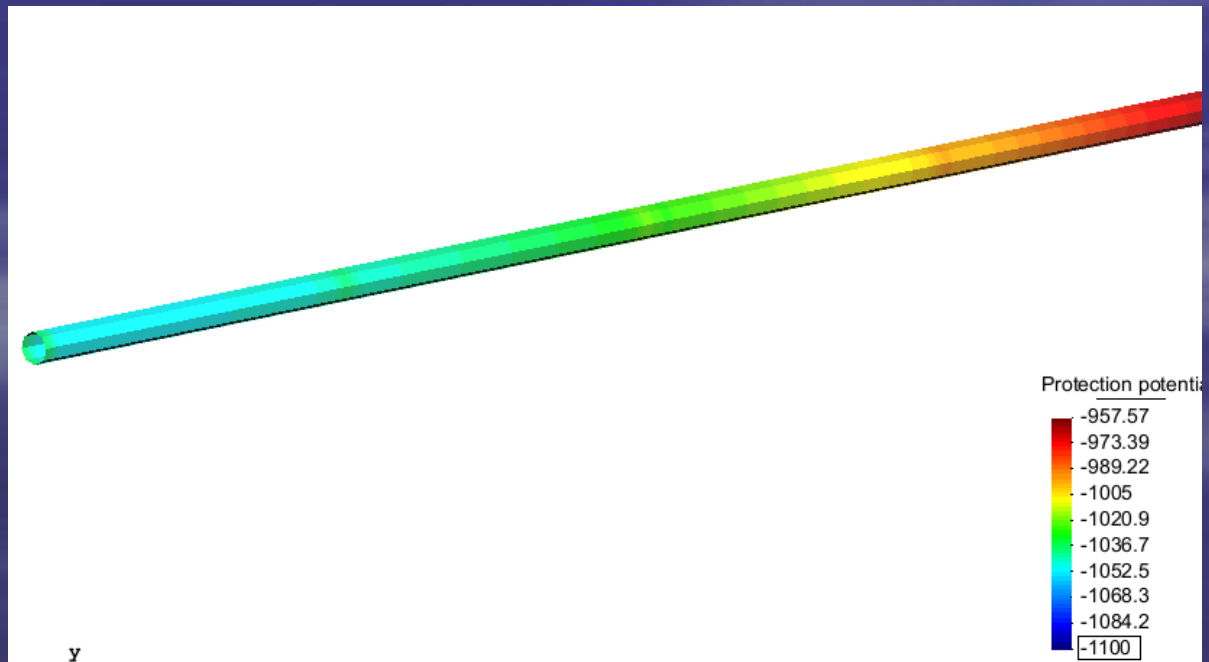
# CP of steel in concrete – global scale

- For a PCCP structure the local investigation used:



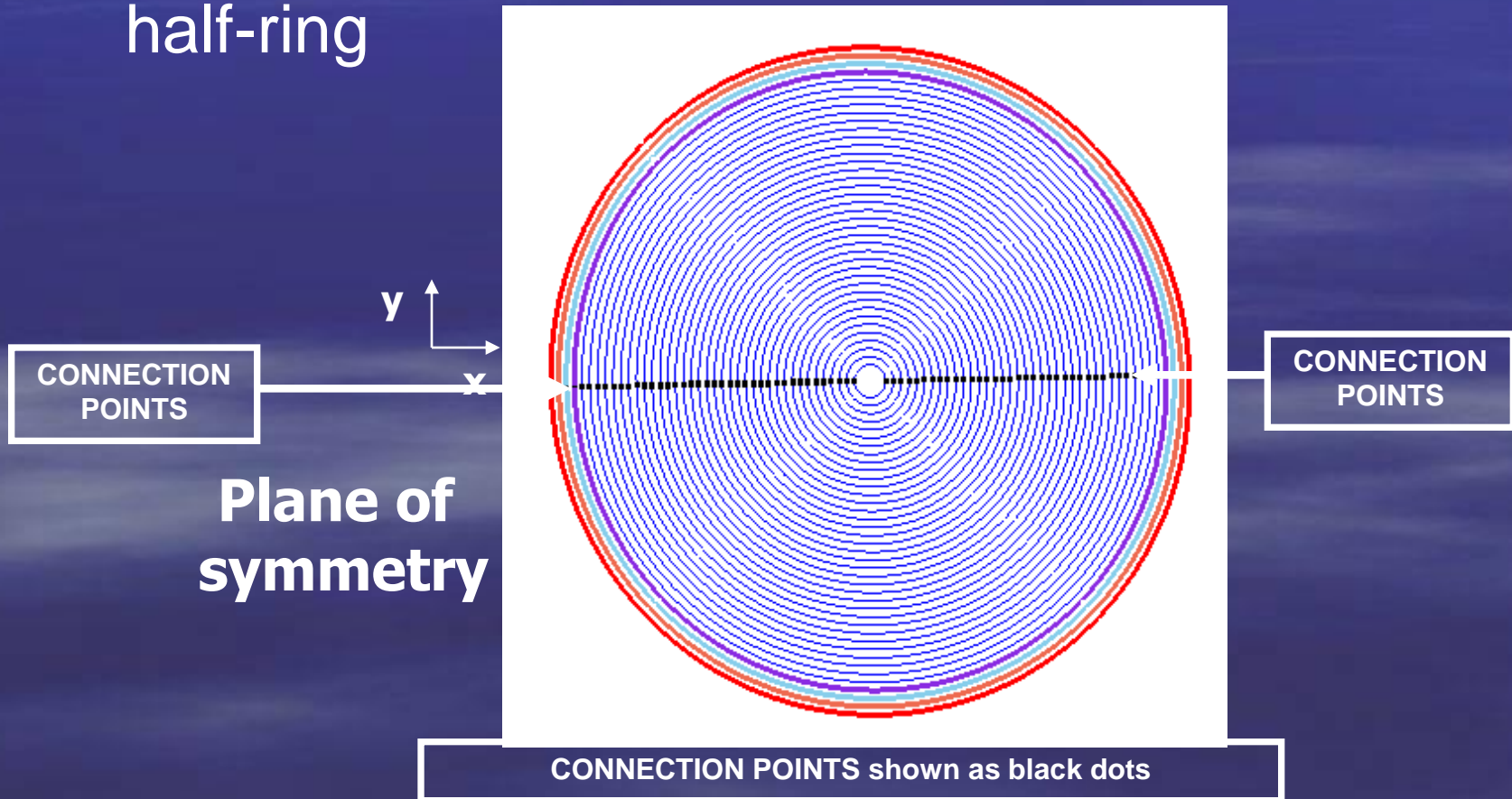
# CP of steel in concrete – global scale

- The PCCP structure was protected by a CP system with linear anodes arranged along the length of the PCCP, but connected only periodically to the pipe
  - Potentials on the PCCP surface can be converted into protection potentials on steel surfaces embedded in concrete/mortar



# Tank base protected by ICCP

- The ICCP system is based on concentric rings of anode ribbons
  - Feeder cables were attached to both ends of each half-ring





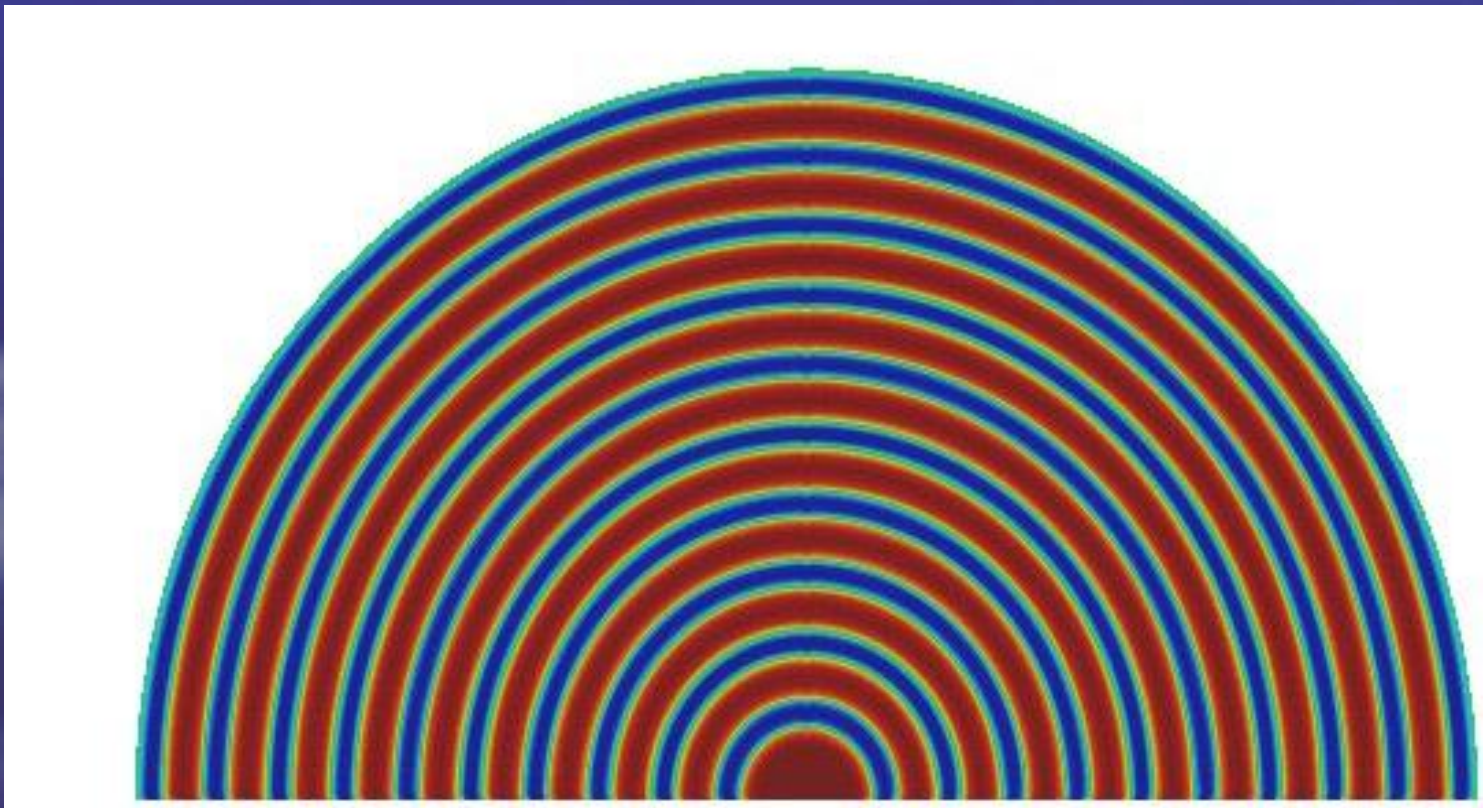
# Tank base protected by ICCP

- The circular tank base has diameter 42 metres, and sits on a 23 cm thick layer of sand below which there is a membrane
- The ribbon anodes:
  - have small cross-section, so large IR drops occur along them in the return path
  - are MMO coated titanium
  - are located 0.06m above the membrane
  - have cross-section 6.35mm by 0.635mm



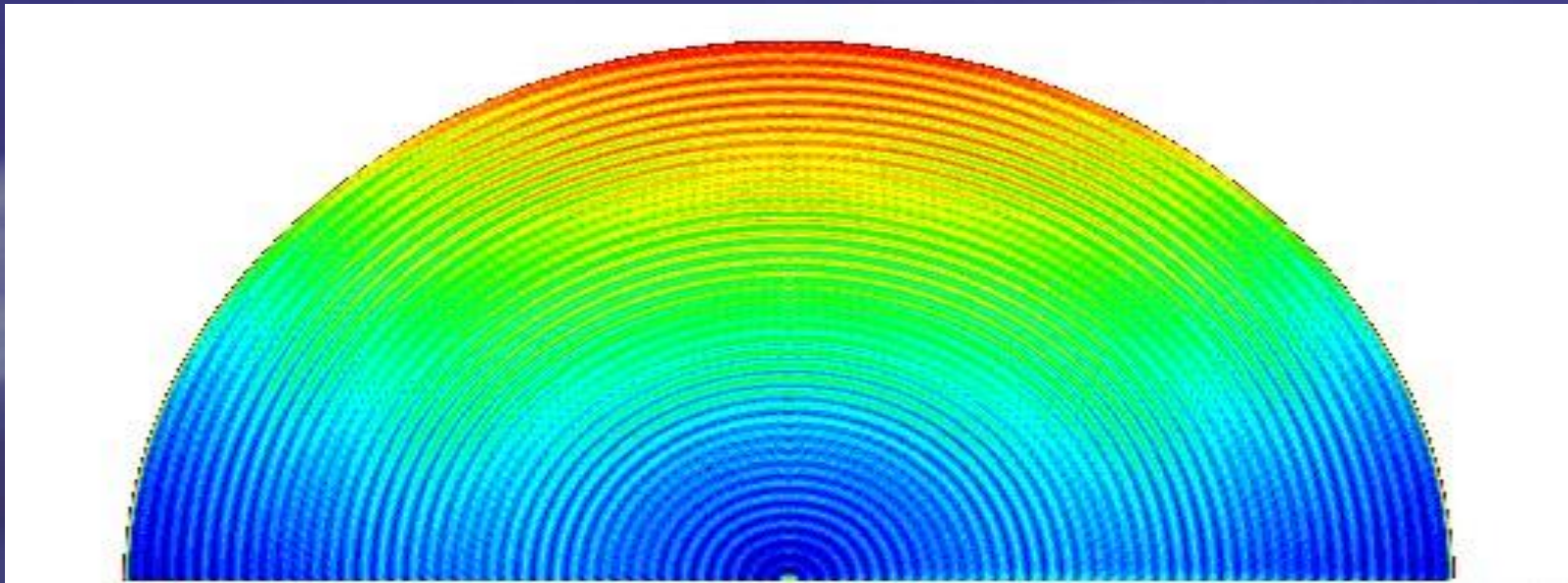
# Tank base ICCP system optimisation

- Potentials on the tank base are not within the target range, even with maximum TRU output



# Tank base ICCP system optimisation

- A revised design using 41 anode rings was assessed
- There was significant variation on the tank base, but potentials are within the target range



# Deep well casings

- **Protection of deep well casings is made difficult by:**
  - **Significant IR drop along the well casing**
  - **Layers of ground which have relatively high/low resistivity**
  - **The need to place anodes at or close to the seabed or ground surface**
- **Simulation allows these influences to be investigated**

# Effect of multiple wells

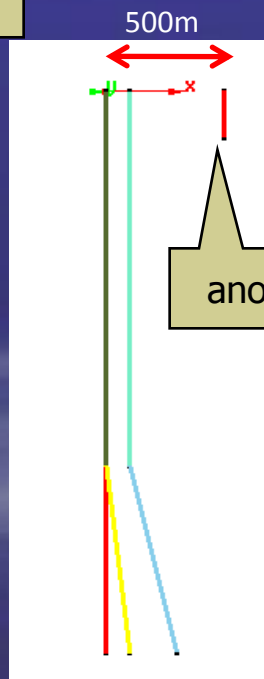
- We first investigate an array of wells in two rows, with a single anode ground bed
- Here the ground is assumed to be homogeneous

Plan view



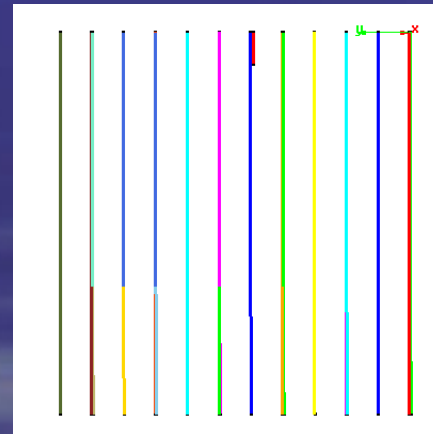
anode

View A

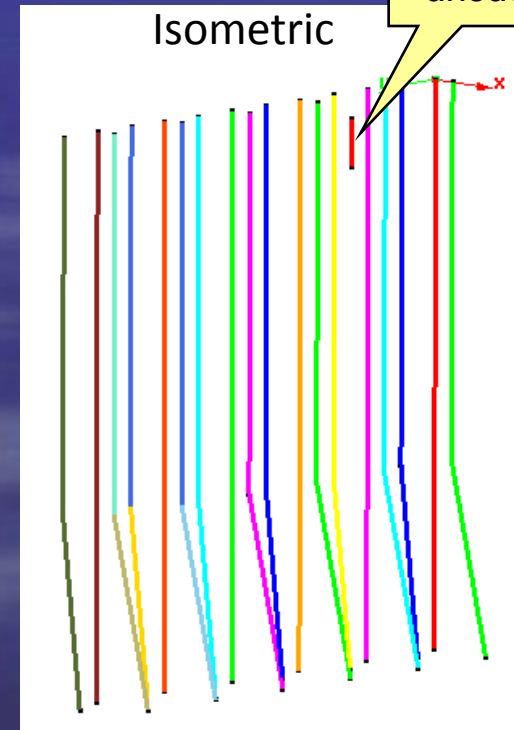


anode

View B



Isometric

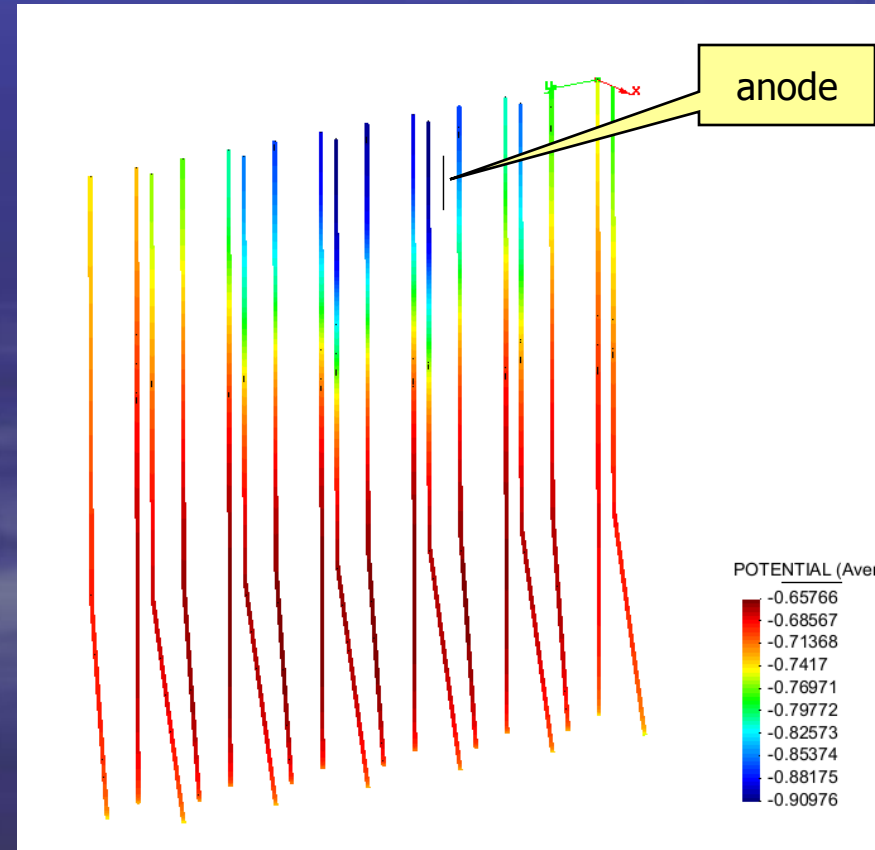


anode

View A

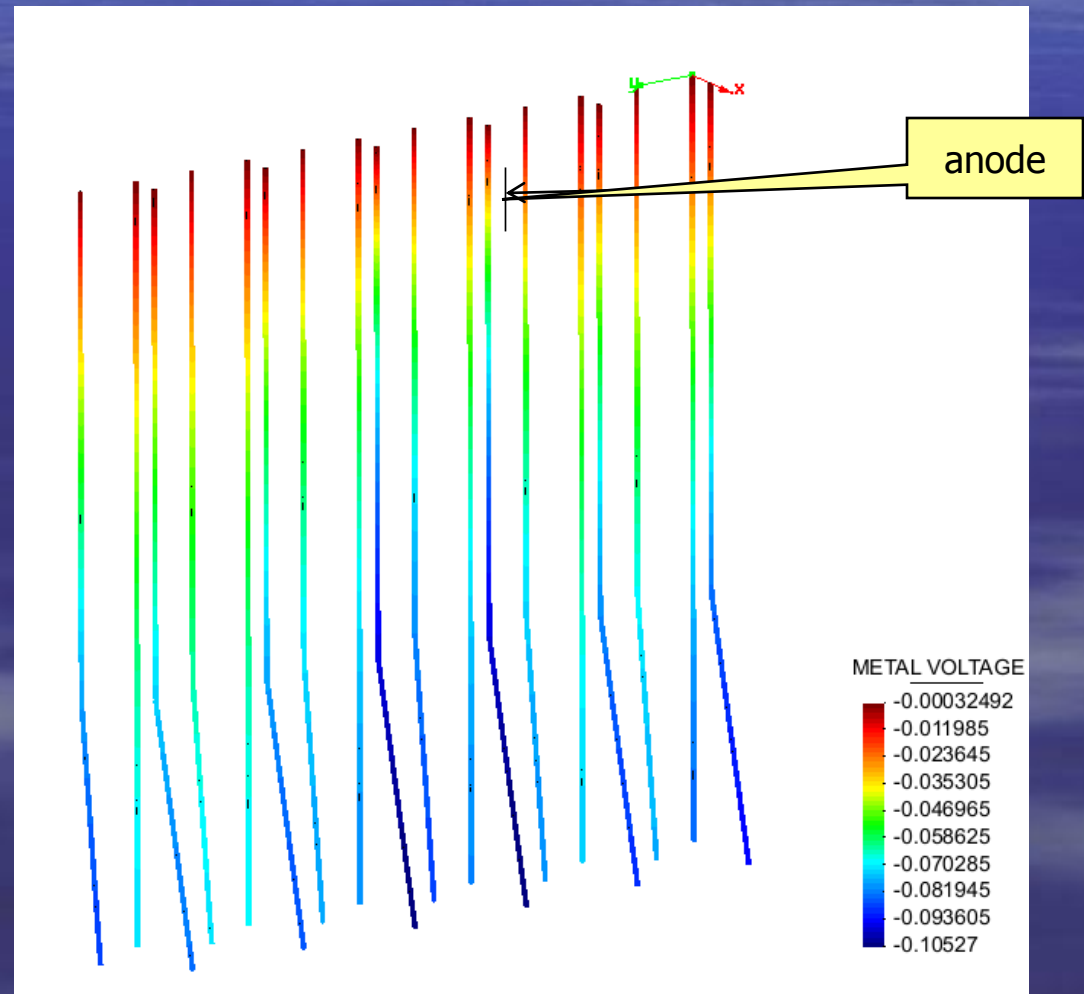
# Potentials on the well casings

- Most negative potential is at the top of the well casings which are closest to the anode
- Significant negative potentials extend to greater depth down the wells in the row closer to the ground bed
- The well furthest from the anode (shown on the left) is better protected than the well next to it, because it receives “end-effect” current



# IR drop along the well casings

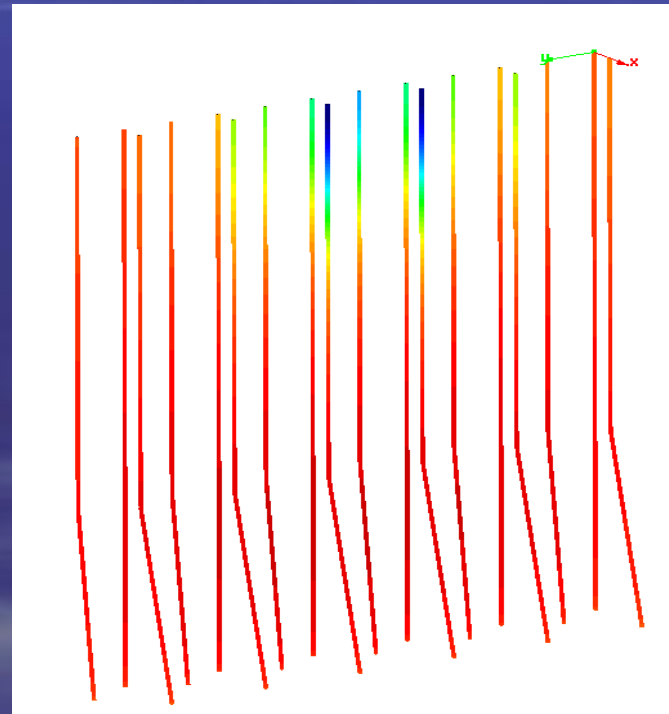
- This contour plot of metal voltage shows that greatest IR drop occurs in the wells nearest to the anode (because these wells receive more current)





# Current density on the deep well casings

- Blue shows biggest current density

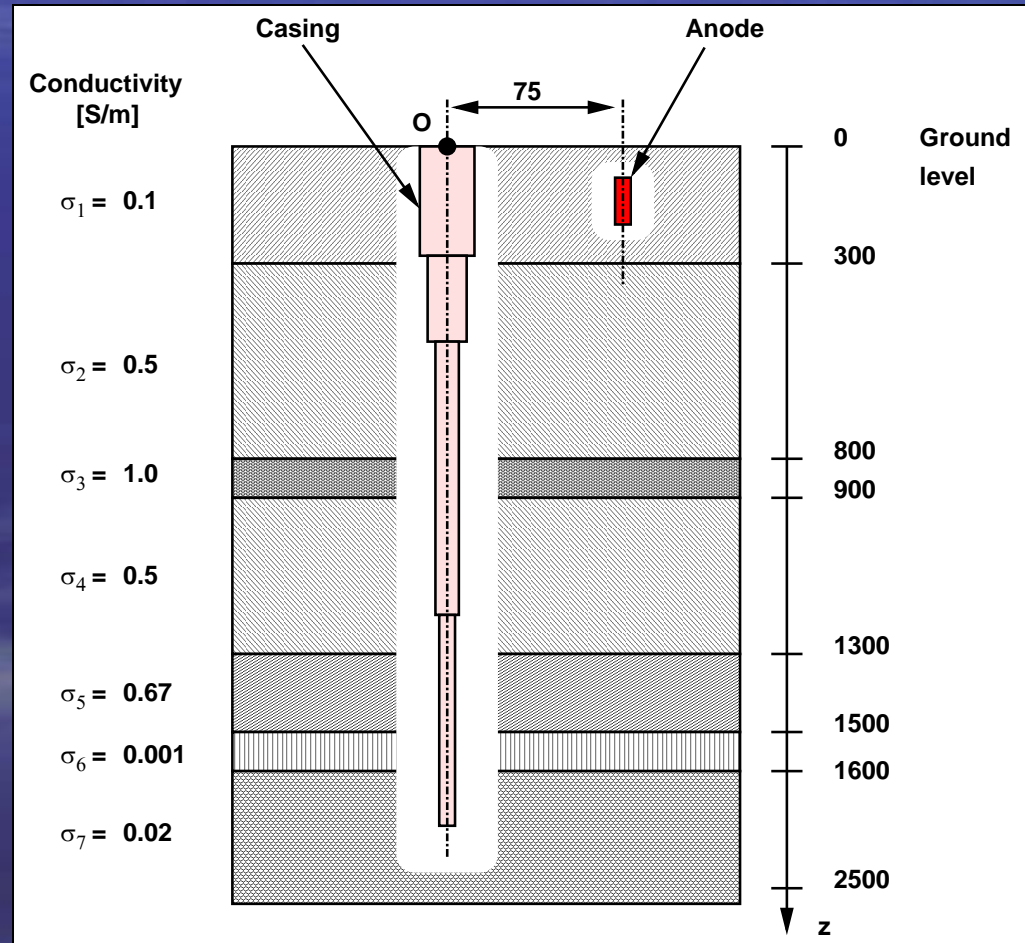


# Anodes protecting arrays of deep well casings

- **Conclusion:**
- **The complex geometry of *arrays* of well casings has a significant effect on achieved protection potential**
  - **Simulation is essential for understanding and control of protection potentials**

# Deep well casings in layered ground

- When multiple ground layers are present, the situation is also complex
- Here we investigate a single vertical well casing
- The anode output is fixed at 10 Amps\*



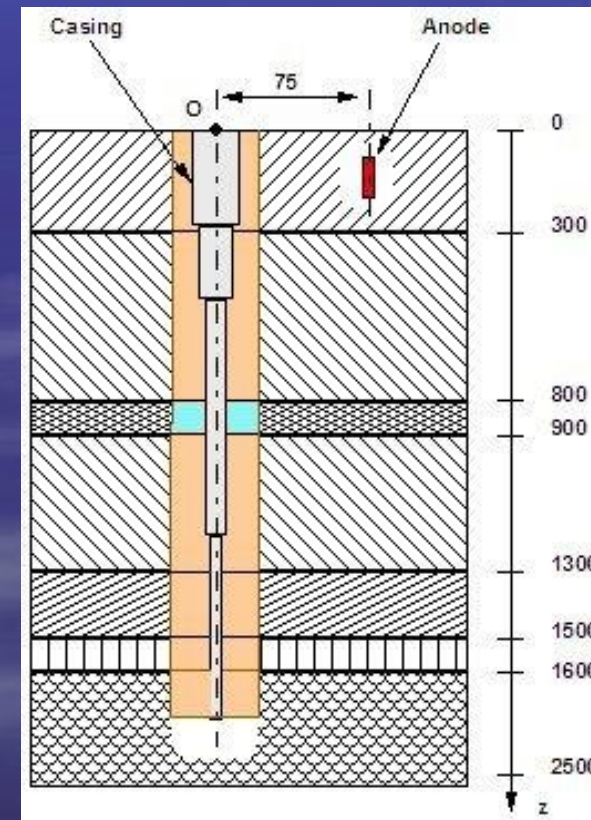
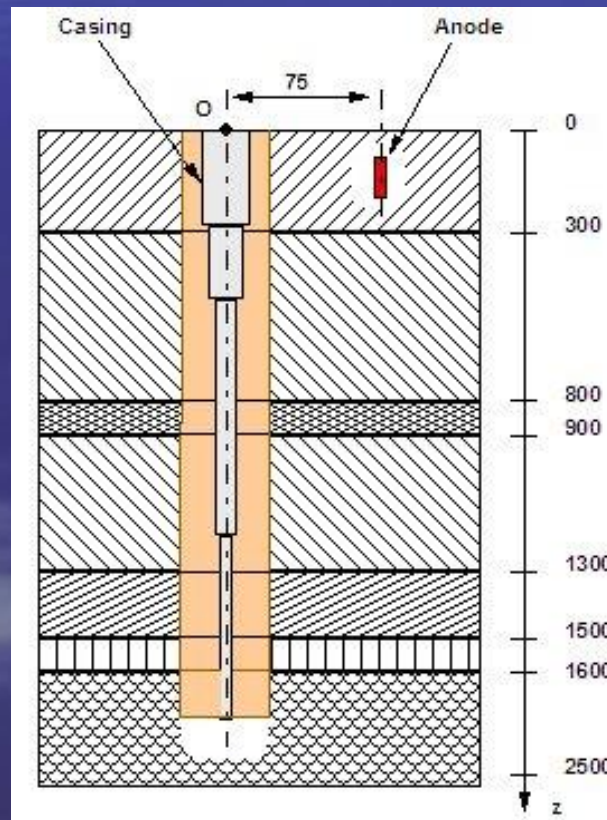
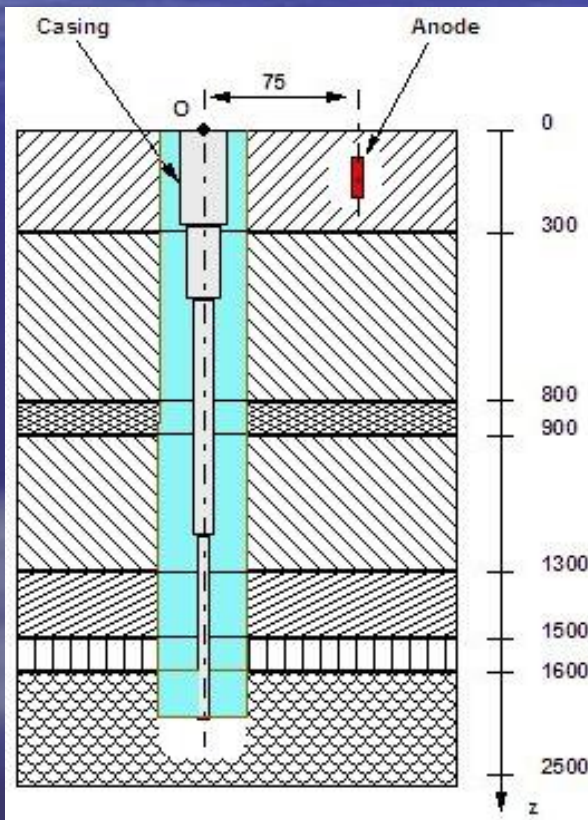
\* A thorough investigation using BEASY was reported by Roche, Vittonato and Jebara in "Cathodic Protection Modeling of Deep Well Casing by 3D software Simulation: Comparison with E-LogI and CPET Data", NACE Corrosion 2008 Conference, Paper number 08273

# Different assumed well cementation

**WET**

**DRY**

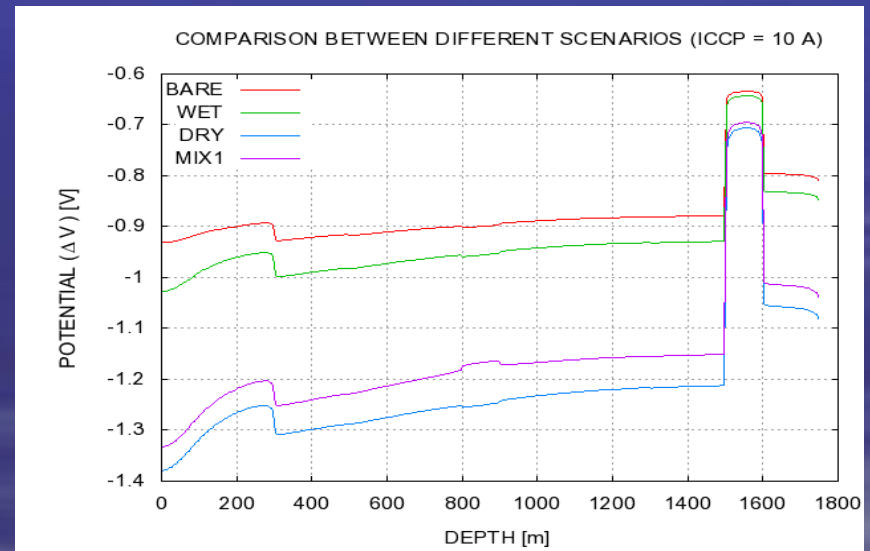
**MIXED**



Sketches are not to scale

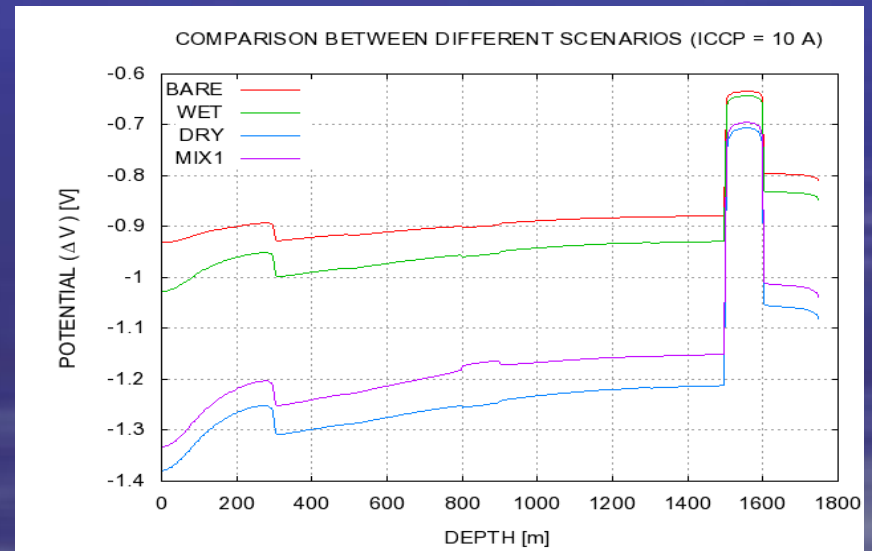
# Potential on the well casing

- The IR drop per metre length of the casing is biggest at the top where current along the casing is greatest
- Protection potential changes rapidly at layer boundaries where resistivity changes significantly



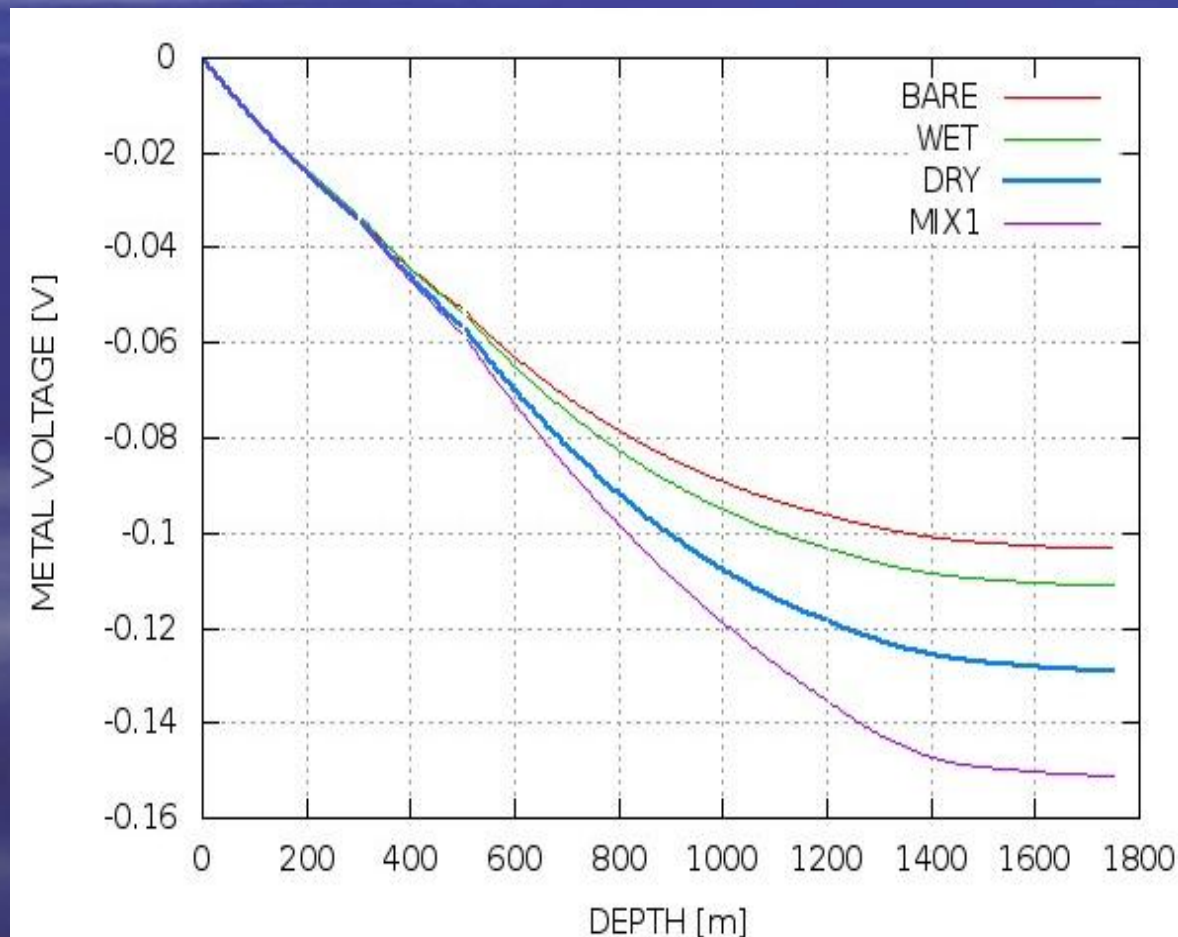
# Potential on the well casing

- There is a ~300mV difference between the “Dry” and the “Wet” cement condition over the majority of the casing
- In the layer just above 1600m depth, where the conductivity is very low (ie resistivity is very high), it is not easy to produce a potential shift
- The layer below however receives current which has travelled vertically through the resistive layer and then horizontally to reach the casing



# IR drop along the casing

- IR drop along the casing is 150 mV for the “MIX1” state of cementing



# Conclusions

- **This paper has shown:**
  - **how computer modelling simulation techniques can be applied to the Design, Optimisation and Operation of CP systems**
  - **That the situations to which simulation can be applied include jacket structures, reinforced concrete structures, ships/FPSOs, pipelines, storage tank bases, deep well casings, etc**
  - **That simulation can be used with sacrificial systems, ICCP systems**
  - **That CP simulation has a beneficial role to play in asset management**



# Conclusions

- **The key demonstrated benefits are:**
  - **Retrofit requirement can be successfully reduced. Hence, significant cost savings achievable**
  - **Better CP current distribution can be obtained despite reduction of number of anodes by better strategic anode positioning**
  - **Assured targeted life extension of the CP system**
  - **Optimized future CP survey frequency is possible. Hence, costs of needless future surveys can be saved**
  - **Improved planning of retrofits and surveys**
  - **Clearly these techniques are of interest to practical CP design for achieving optimization and cost saving**